Eigenvalue Analysis of 2D Helmholtz Equation on Quadrilateral Elements

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I. Introduction

Eigenvalue analysis is one of the most important and fundamental tools for wave and vibration, and has been treated by the finite element method (FEM) $[1 - 6]$, by the boundary element method (BEM) [7, 8], and also by the integral equation [9]. In this paper we study the Helmholtz equation which governs the time-harmonic wave problem $(\nabla^2 + k^2)u = 0$, since $k = 2\pi/\lambda$, where *k* is the wave ∂ number and λ is the wave length, and u is the field of interest which could be wave elevation, pressure, or an electro-magnetic potential, among many other possibilities [3]. Recently the same problem was considered by the method of the special integration scheme [3, 4] and the theory of integrations of the element matrices for rectangular, triangular and special quadrilateral finite elements for very short waves, and they used Maple and FORTRAN codes for the evaluation of integration abscissas and weights. Ortiz and Sanchez [5] also developed an analytical integration procedure for their triangular elements. They applied local co-ordinate rotation to the integrand so that the oscillatory component is transformed into the form depending only on one 'effective' direction with an 'equivalent' wave number. This simplifies the integration procedure and reduces the number operations. Hacker and Schreyer [6] studied exact analytical expressions for the eigenvalues only for four node rectangular elements. The quadrilateral element is more complicated to deal with than rectangular or triangular element due to the $\xi \eta$ term in the Jacobian. Thus the objective of this study is to evaluate the eigenvalue analysis for general quadrilateral elements and finally a comparison is made with the exact solutions.

II. FE Formulation of Helmholtz Equation

The partial differential equation (PDE) governing transient heat transfer on a 2-D region Ω

$$
c \frac{\partial u}{\partial t} - \frac{\partial}{\partial x}(a_{11} \frac{\partial u}{\partial x}) - \frac{\partial}{\partial y}(a_{22} \frac{\partial u}{\partial y}) + a_0 u = f(x, y, t)
$$
 (1a) where a superposed dot on u denotes the time derivative

with the boundary conditions (b.c.),

$$
u = u, q_n = a_{11} \frac{\partial u}{\partial x} n_x + a_{22} \frac{\partial u}{\partial x} n_y = q_n \text{ on } \gamma
$$

(1b)
$$
M_{ij}^e = \iint_e c \, u_i v_j
$$

$$
K_{ij}^e = \iint_e (a_{11} \frac{\partial w}{\partial x})^2 dx
$$

and the initial conditions (i.e. at $t = 0$) are of the form

$$
u(x, y, 0) = u_0(x, y) \text{ in } \Omega \tag{1c}
$$

Here *t* denotes the time and $c, a_{11}, a_{22}, a_0, u_0, f, \hat{u}, \hat{q}_n$ are given as functions of position and/or time.

The corresponding homogeneous boundary value problem is

$$
c\frac{\partial u}{\partial t} - \frac{\partial}{\partial x}(a_{11}\frac{\partial u}{\partial x}) - \frac{\partial}{\partial y}(a_{22}\frac{\partial u}{\partial y}) + a_0 u = 0 \text{ in } \Omega
$$
 (2a) Assuming the element equations (9), we have

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$$
u = 0 \t q_n = 0 \t on \t \gamma \t (2b)
$$

Solution of equation (2) is known generally to behave according to

$$
u(x, y, t) = \psi(x, y) \exp(-\beta t)
$$
 (3)

which reduces equation (2) as

$$
\frac{\partial}{\partial x}(a_{11}\frac{\partial \psi}{\partial x}) + \frac{\partial}{\partial y}(a_{22}\frac{\partial \psi}{\partial y}) + \lambda \psi = 0
$$
 (4a)

where $\lambda = c\beta + a_0$ and the b.c. (2b) reduces to

$$
\psi = 0, \, \partial \psi / \partial \eta = 0 \tag{4b}
$$

The λ 's and ψ 's satisfying eqs. (4) are known as *eigenvalues* and *eigenfunctions*, respectively. The differential equation (4), which represents the *timeindependent* form of original equation, results from applying the technique of separation of variables to reduce the complexity of the analysis, is known as the *Helmholtz equation*.

The weak form of (1) over an element [*e*] is obtained by substituting a finite element approximation for the dependent variable *u* as

$$
u(x, y, t) \approx \sum_{j=1}^{n} u_j^e(t) \psi_j^e(x, y)
$$
 (5)

where u_j denotes the value of $u(x, y, t)$ at the spatial location (x_j, y_j) at time *t*.

The *i*-th element equation (in time) of the finite element model is

$$
\sum_{j=1}^{n} (M_{ij}^e \frac{du_j^e}{dt} + K_{ij}^e u_j^e) = f_i^e + Q_i^e
$$
 (6)

or in matrix form,

$$
[M^e]{\{u^e\}} + [K^e]{\{u^e\}} = {f^e}{\{Q^e\}}
$$
 (7)

 $(i = du/dt)$ and

$$
M_{ij}^{e} = \iint_{e} c \psi_{i} \psi_{j} dx dy, f_{i}^{e} = \iint_{e} f \psi_{i} dx dy, Q_{i}^{e} = \int_{\tau^{e}} q_{n} \psi_{i} ds
$$

$$
K_{ij}^{e} = \iint_{e} (a_{11} \frac{\partial \psi_{i}}{\partial x} \frac{\partial \psi_{j}}{\partial x} + a_{22} \frac{\partial \psi_{i}}{\partial y} \frac{\partial \psi_{j}}{\partial y} + a_{0} \psi_{i} \psi_{j}) dx dy
$$
 (8)

The matrices K_{ij}^e and M_{ij}^e are known as element matrix and mass matrix, respectively.

Substituting $u_j^e(t) = u_j \exp(-\lambda t)$ in (7) to obtain,

$$
(-\lambda [M^e] + [K^e])\{U\} = \{0\}
$$
\n⁽⁹⁾

$$
([K] - \lambda[M])\{U\} = \{0\} \tag{10}
$$

A non-trivial solution to equation (10) exists only if $|[K] - \lambda[M]| = 0$, which when expanded results in an *n*-th degree polynomial in λ , where *n* is the number of nodes at which the solution is not known. The *n* roots, λ_j , $j = 1, ...,$ *n* of this polynomial gives the first *n eigenvalues* of the increased system.

III. Numerical Example

For the well-known transient heat conduction equation, the following PDE is considered [1],

$$
\frac{\partial u}{\partial t} - \nabla^2 u = f \tag{11}
$$

in a square region $D = \{(x, y) : 0 < x < 1, 0 < y < 1\}$, subject to the boundary conditions for $t > 0$, shown in Fig. 1.

$$
\frac{\partial u}{\partial t}(0, y, t) = 0, \frac{\partial u}{\partial y}(x, 0, t) = 0,
$$
\n
$$
u(x, 1, t) = 0, u(1, y, t) = 0
$$
\nand the initial condition\n
$$
u(x, y, 0) = 0.
$$
\n
$$
u(x, y, 0) = 0.
$$

The homogeneous form of (11) is, **Fig 1**. Domain *D*

$$
\frac{\partial u}{\partial t} = \frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2}
$$
 (12a)

with boundary conditions,

$$
\frac{\partial u}{\partial t}(0, y, t) = 0, \quad \frac{\partial u}{\partial y}(x, 0, t) = 0,
$$
\n
$$
u(x, 1, t) = 0, u(1, y, t) = 0
$$
\n(12b) result

The exact solution of (12) is

$$
u(x, y, t) = T_0 \exp(-\lambda t)U(x, y)
$$

\n
$$
= T_0 \exp(-\lambda t)(c_1 \sin \sqrt{\mu x} + c_2 \cos \sqrt{\mu x}) \times
$$

\n
$$
(c_3 \sin \sqrt{\lambda - \mu} y + c_4 \cos \sqrt{\lambda - \mu} y)
$$

\n2. Bickford, W. B. (1990) - A First Course in the Finite Element
\nMethod, Second Edition, Irwin.
\n3. Bettes , P., Shirron, J., Laptrouche, O., Peseux, Bernard

where λ is the required eigenvalue and the nontrivial $U(x, y)$ is the corresponding eigenfunction. The exact [1] eigenvalue λ is $\lambda_{m,n} = \pi^2 (m^2 + n^2)/4$, $m, n = 1, 3, 5, ...$ 4. Sugimoto, R., B

Now we evaluate the approximate eigenvalues using the mesh of quadrilateral elements, shown in Fig. 2.

Fig. 2. Different Mesh of the domain of the problem.

The eigenvalues are calculated using the present formulation and compared to the exact solutions. The errors $(\%)$ are 9 . shown in Table 1.

Table. 1. Errors (%) analysis for the meshes in Fig.2.

	Mesh1		Mesh 2			Mesh 3			Exact
Q ₄	Q8	Q ₉	Q4	Q8	Q ₉	Q4	Q8	Q ₉	
21.59	1.1	0.75	5.24	0.05	0.28	4.53	27.54	16.15	04.935
\sim			40.5 40.5 38.95	3.1	2.89	36.67	1.64	1.63	24.674
$\overline{}$	44.6		40.5 38.95	3.1	3.61	2.11	16.35	13.36	24.674
$\overline{}$	--	--	$-$	8.29	3.05	۵.	13.83	12.44	44.413
\ddotsc	--	0.32	1.21	\overline{a}	--	$11.01 -$		\sim	64.152
\sim	--	--	--	5.07	5.97	\overline{a}	1.98	3.14	83.892
$\overline{}$	--	--	-1	5.07	5.05	\overline{a}	2.76	2.33	83.892
$\overline{}$	--	--	--	18.93	18.97	\overline{a}	\overline{a}	21.01	123.370
\sim	--	--	--	6.54	18.34	$-$	\overline{a}	--	123.370
\overline{a}	--	--	$-$	\overline{a}	7.18	\overline{a}	8.81	\sim	143.109
$\overline{}$	--	--	--	--		--	9.12	\sim \sim	143.109
\sim	--	--	-1	0.57	1.87	$-$	0.83	0.81	202.327
\sim	--	--	$-$	0.44	0.47	$-$	1.16		202.327
	--	--	--	3.74	1.30	--	--	--	222.066
$\overline{}$	--	--	$-$	3.74	0.13	$-$	$-$	9.57	222.066
\sim	--	--	$-$	\overline{a}	$-$	$-$	1.54	1.56	261.544
	--	--	--	--	5.16	--	--	1.56	261.544
\sim	--	--	--	--	7.32	$-$	$-$	1.56	261.544
\sim	--	--	--	--	--	--	--	0.09	301.023
$-$	--	--	--	--	3.98	--	--	5.49	419.458

IV. Conclusions

x

(12a) *MATHEMATICA*. We observe that regular Q8 elements give $r = 0$, $r = (12k)$ results with high accuracy. In this paper the eigenvalue analysis of Helmholtz equation using FEM over quadrilateral element is studied. Two types finite elements, such as regular and distorted quadrilateral, are discussed. All integrals of the element matrices and mass matrices are evaluated analytically using better results than those of distorted quadrilateral elements for small eigenvalues. On the other hand, for largest eigenvalues, Q9 elements may be recommended to get the

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